

## EE752 Homework#1 Solution

2-1

With  $h_0$  is an equilibrium point for the system with input  $\mu_0$ , ( $\dot{h}(t) = f(h_0, u_0) = 0$ ).

Around this equilibrium point, linearize the system with respect to the first order Taylor's series.

$$\delta \dot{h}(t) = \dot{h}(t) \approx f(h_0, u_0) + \left. \frac{\partial f}{\partial u} \right|_{u_0} \delta u(t - \tau) + \left. \frac{\partial f}{\partial h} \right|_{h_0} \delta h(t)$$

where  $\left. \frac{\partial f}{\partial u} \right|_{u_0} = \frac{1}{A_0}$  and  $\left. \frac{\partial f}{\partial h} \right|_{h_0} = \frac{V_0}{2A_0\sqrt{h_0}}$ , substitute into equation above and apply Laplace

Transform, we will obtain,

$$G(s) = \frac{\delta h(s)}{\delta u(s)} = \frac{e^{-s\tau}}{A_0(s + \frac{V_0}{2A_0\sqrt{h_0}})}$$

2-2

(i)  $\tau = 0$

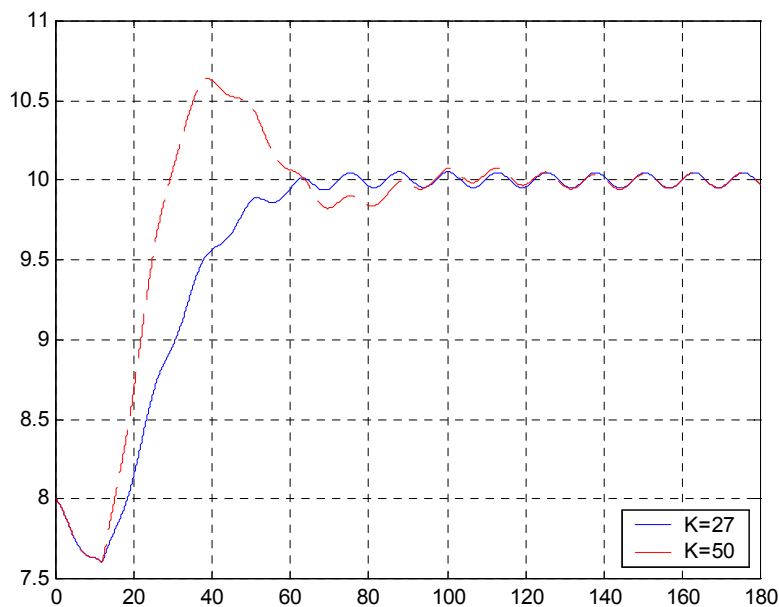
The system dynamics  $\dot{h} = \frac{u(t) - v(t)}{A(h(t))}$

$v(t)$  is known, define  $u'(t) = u(t) - v(t)$ . Since we need  $h(t) \rightarrow h_d(t)$  as  $t \rightarrow \infty$ , the designed dynamics could be  $\mu \dot{h}(t) + h(t) = h_d(t)$ ,  $\mu > 0$  ( $h(t) \rightarrow h_d(t)$  with  $\mu \rightarrow 0$ , what if  $\mu < 0$ ?).

To achieve the designed dynamics, choose  $u'(t) = \frac{A(h(t))}{\mu}(-h(t) + h_d(t))$  with small  $\mu$

(why?).

(ii)



Matlab code:

```
clear all;

% Given constants
A0=300;
A1=12;
A2=120;
Tao=12; % the time delay
v0=24;
h_d=10;
h_0=8;
% Feedback gain to be designed
K_min=27; % lower bound for K
K_max=50; % upper bound for K
% Initialize the simulation
Ts=0.04;
t=0:Ts:180;
N=length(t); % number of simulation steps
step_of_delay=Tao/Ts;
% Using Euler's first order method: X(k+1)=X(k)+Ts*f(k)
h_1=zeros(size(t)); % Initialize h vector for K_min case
h_1(1)=h_0;
h_2=zeros(size(t)); % Initialize h vector for K_max case
h_2(1)=h_0;
for i=2:N,
    if i<=step_of_delay
        u1=0; % control for K_min case
        u2=0; % control for K_max case
    else
        u1=K_min*(h_d-h_1(i-step_of_delay))+v0; % control for K_min case
        u2=K_max*(h_d-h_2(i-step_of_delay))+v0; % control for K_max case
    end
    h_1(i)=h_1(i-1)+Ts*(u1-(v0+20*sin(0.5*t(i-1))))/(A0+A1*h_1(i-...
    1)+A2*sqrt(h_1(i-1)));
    h_2(i)=h_2(i-1)+Ts*(u2-(v0+20*sin(0.5*t(i-1))))/(A0+A1*h_2(i-...
    1)+A2*sqrt(h_2(i-1)));
end
% Plot the results:
figure(1)
plot(t, h_1, 'b-', t, h_2, 'r--');grid on;zoom on;
legend('K=27', 'K=50', 4);
```

You can compare the performance of different Ks by using the code above.

2-5

The transfer function between disturbance  $v(t)$  and output  $y(t)$  is  $\frac{P(s)}{1+P(s)C(s)}$ .

Because this is a linear system, the output is the superposition from the input and the disturbance. Now consider the part of the output from the disturbance.

$$y_v(s) = \frac{P(s)}{1+P(s)C(s)} v(s) = \frac{P(s)}{1+P(s)C(s)} \frac{3}{s^2+9} \quad (*) \quad [\text{because } v(t) = \sin(3t)].$$

From  $y(t) \rightarrow 0$  as  $t \rightarrow \infty$ , we have  $y_v(t) \rightarrow 0$  as  $t \rightarrow \infty$ .

Thus, in (\*),  $s^2+9$  must be eliminated from the denominator. Otherwise, after the partial expansion, we know there will always be some sinusoidal components in the output.

To cancel  $s^2+9$ , it is clear that the controller  $C(s)$  must have  $s^2+9$  term in the denominator.